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1. 



NUCLEAR INSTRUMENTS \& METHODS IN PHYSICS
RESEARCH
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EMMA: A recoil mass spectrometer for ISAC-II at TRIUMF

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Available online 11 March 2005
2. The EMMA settings example and apertures kindly provided by Matt Williams (TRIUMF)

## LISE ${ }^{++}$package / files



## LISE ${ }^{++}$package / configurations

| LISElconfig\TRIUMF** |  |  |  |
| :---: | :---: | :---: | :---: |
| Name | Ext | Size | $\downarrow$ Date |
| ¢ $4 . .1$ |  | <DIR> | 11/17/2015 |
| - EMMA | Icn | 112.029 | 11/17/2015 |
| [ ${ }_{\text {F }}$ s_DRAGON2000 | Im | 34.35 | 07/22/2015 |
| 言e_DRAGON2000 | Icn | 329.08 | 07/22/2015 |

LISE++ site / 9_10/ EMMA


Index of /9_10/EMMA

| Name | Last modified | Size |  |
| :--- | :--- | :--- | :--- |


| Block |  | Given Name | Start(m) | Length(m) | B0 $(\mathrm{kG}) / \times \mathrm{L}$ | $\mathrm{Br}(\mathrm{Tm}) \mathrm{cor} /$ /real | DriftM/*Angle | Rapp $(\mathrm{cm}) / \times \mathrm{R}(\ldots$ | Leff(m)/*Ldip(m) | 2 nd order | CalcMatr/ $/ 2-Q$ | AngAcc,Apps, Slits | COSY/Fit | SE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D) | = Dipole | tuning | 0.000 | 0.0001 | +3.2873 | * 0.9862 | ${ }^{*}+0.0$ | $\times 3.0000$ | * 0.0000 | . | * 19 | HV .. .- | . | S |
| da | drift | Drift 1 | 0.000 | 0.2470 |  |  | standard |  |  |  |  | .. HV .- | - | e |
| $Q>$ | <Quad> | Q1 | 0.247 | 0.1398 | +13.4745 | 0.9862 | QUAD | 3.5000 | 0.1398 | yes | 1 R | .. HV .- | . | e |
| da | drift | drift Q12 | 0.387 | 0.0350 |  |  | standard |  |  |  |  | .. HV .- | - | e |
| $Q>$ | <Quad> | Q2 | 0.422 | 0.2988 | -8.7698 | 0.9862 | QUAAD | 7.5000 | 0.2988 | yes | 1 R | .- HV -- | - | e |
| d민 | difit | difit Q2E | 0.721 | 0.3723 |  |  | standard |  |  |  |  | .- HV .- | - | e |
| E | =ElecDip | ElecDip 1 | 1.093 | 1.7453 | ${ }^{*} 546.4 \mathrm{kV}$ | 0.9862 | * +20.0 | * 5.0000 | * 1.7453 | - | * 19 R | .- HV .- | - | E |
| dㅁ | difit | drift ED | 2.838 | 1.2250 |  |  | standard |  |  |  |  | .. HV .- | - | e |
| D) | $=$ Dipole | DipoleA | 4.063 | 0.3491 | $-9.8619$ | * 0.9862 | * -20.0 | $\times 1.0000$ | * 0.3491 | yes | * 19 R | .. .. .. | - | E |
| S III | _silis_ | dip slits | 4.412 | 0.0000 |  |  | SLITS |  |  |  |  | .. .. HV | - | e |
| D) | $=$ Dipole | DipoleB | 4.412 | 0.3491 | -9.8619 | * 0.9862 | * -20.0 | * 1.0000 | * 0.3491 | yes | * 19 R | -. .- | - | E |
| d미 | difift | drift DE | 4.761 | 1.2225 |  |  | standard |  |  |  |  | .. HV .- | - | e |
| E- | =ElecDip | ElecDip 2 | 5.984 | 1.7453 | ${ }^{*} 546.4 \mathrm{kV}$ | 0.9862 | * +20.0 | * 5.0000 | * 1.7453 | - | * 19 R | .- HV -- | - | E |
| dロ | drift | drift EQ3 | 7.729 | 0.3649 |  |  | standard |  |  |  |  | .- HV .- | $\cdot$ | e |
| $Q>$ | <Quad> | Q3 | 8.094 | 0.2988 | $-5.7122$ | 0.9862 | QUAAD | 7.5000 | 0.2988 | yes | 1 R | .- HV -- | fit - Q | e |
| d $\square$ | drift | drift Q34 | 8.393 | 0.0300 |  |  | standard |  |  |  |  | .- HV .- | - | e |
| $0 \vee$ | <Quad> | Q4 | 8.423 | 0.4018 | +6.8799 | 0.9862 | QUA, | 10.0000 | 0.4018 | yes | 1 R | .. HV .- | fit - Q | e |
| dㅁ | drift | drift Q4FP | 8.825 | 0.3076 |  |  | standard |  |  |  |  | .- HV -- | . | e |
| S II | _silts_ | FP slits | 9.132 | 0.0000 |  |  | SLITS |  |  |  |  | .. .. HV | - | e |

All "E"-blocks.
Extended configuration
$\overline{7}$ Quads \& Dipoles settings

symbol "*" after values denotes, that these values belongs to Dipole settings, where column names are found in the second row
Column 08: "Br-corrsp" - quadrupole(sextupole) field is scaled to this Brho-value; "Br-dip*" - dipole magnetic rigidity [T*m]
Column 08: "Br-corrsp" - quadrupole(sextupole) field is scaled to this Brho-value; "Br-dip*" - dipole magnetic
Column 09: "Rapp(cm)" - radius(half-aperture) of quadrupole(sextupole) in cm; "R(m)-dip*" - dipole raidus [m]
 Column 12: "Calc mode" - only for quadrupole(sextupole): 0 - no actions; 1 - recalculate automatically $B(f i e l d)$, keep matrix;

2- recalculate automaticall
Colums 15-18,20-23: slits and aperture(limit) sizes in [mm. If slit or aperture(limit) does not have action, then its size value is abser

These aperture parameters are used to obtain angular and momentum acceptances of the separator.

- LISE++ does not provide information for mass dispersion
- So, this value can not be used for optimization constraint
- Quad values have been taken from EMMA beam example
- All matrices have been calculated inside LISE ${ }^{++}$


## EMMA_beam__original.Ipp

| Block |  | Given Name | Start(m) | Length(m) | $80(k G) / \times \mathrm{U}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D | = Dipole | tuning | 0.000 | 0.0001 | +3.2207 |
| d만 | dirit | Difit 1 | 0.000 | 0.2470 |  |
| Q $\triangle$ | <Quad> | Q1 | 0.247 | 0.1398 | +13.2014 |
| d口 | dirit | dift Q12 | 0.387 | 0.0350 |  |
| Q $\triangle$ | <Quad> | Q2 | 0.422 | 0.2988 | -8.8066 |
| dㅁ | difit | difit Q2E | 0.721 | 0.3723 |  |
| E | =ElecDip | ElecDip 1 | 1.093 | 1.7453 | *450.2kV |
| dㅁ | dirit | drift ED | 2.838 | 1.2250 |  |
| D) | = Dipole | DipoleA | 4.063 | 0.3491 | -9.6620 |
| S II | _sits_ | dip sits | 4.412 | 0.0000 |  |
| D) | = Dipole | DipoleB | 4.412 | 0.3491 | -9.6620 |
| dㅁ | difit | Drift DE | 4.761 | 1.2225 |  |
| E | =ElecDip | ElecDip 2 | 5.984 | 1.7453 | ${ }^{*} 450.2 \mathrm{kV}$ |
| dㅁ | diift | drift EQ3 | 7.729 | 0.3649 |  |
| $Q>$ | <Quad> | Q3 | 8.094 | 0.2988 | -6.0155 |
| dロ | drift | difit Q34 | 8.393 | 0.0300 |  |
| $Q \Delta$ | <Quad> | Q4 | 8.423 | 0.4018 | +7.7544 |
| dㅁ | drift | drift Q4FP | 8.825 | 0.3076 |  |
| S II | _silis_ | FP slits | 9.132 | 0.0000 |  |

Global LISE ${ }^{++}$matrix with these quad values
Note: No Y-focus, large Y/Y value

－LISE＋＋optimization was done to get Y －focus in the middle of M －dipole， X － \＆Y－focuses＠the end，R11 \＆R33 values according to the EMMA paper

## EMMA＿beam＿＿original．Ipp

| Block |  | Given Name | Start（m） | Length（m） | B0（kG1）$\times \mathrm{U}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pr | ＝Dipole | turing | 0.000 | 0.0001 | ＋3．2207 |
| da | dift | Difit 1 | 0.000 | 0.2470 |  |
| $0 \bigcirc$ | ＜Quad＞ | Q1 | 0.247 | 0.1398 | ＋13．2014 |
| $\square$ | difit | difit Q12 | 0.387 | 0.0350 |  |
| Q 0 | ＜Quad＞ | Q2 | 0.422 | 0.2988 | －8．8066 |
| d $\square$ | diit | difit Q2E | 0.721 | 0.3723 |  |
| E | ElecDip | ElecDip 1 | 1.093 | 1.7453 | ＊450．2kV |
| d $\square$ | diit | dirit ED | 2.838 | 1.2250 |  |
| D2 | ＝Dipole | DipoleA | 4.063 | 0.3491 | －9．6620 |
| S II | ＿sits＿ | dip silis | 4.412 | 0.0000 |  |
| Did | ＝Dipole | DipoleB | 4.412 | 0.3491 | 9.6620 |
| d $\square$ | diit | Diitit DE | 4.761 | 1.2225 |  |
| E | EElecDip | ElecDip 2 | 5.984 | 1.7453 | ＊450．2kV |
| d $\square$ | diit | dirit EQ3 | 7.729 | 0.3649 |  |
| Q $\bigcirc$ | ＜Quad＞ | Q3 | 8.094 | 0.2988 | －6．0155 |
| da | dirit | dirit Q34 | 8.393 | 0.0300 |  |
| ${ }^{\circ} \bigcirc$ | ＜Quad＞ | Q4 | 8.423 | 0.4018 | ＋7．7544 |
| d $\square$ | diit | difit Q4FP | 8.825 | 0.3076 |  |
| S III | ＿sitis＿ | FP silis | 9.132 | 0.0000 |  |

## EMMA＿beam．Ipp

| Block |  | Given Name | Start（m） | Length（m） | B0［kG1） 4 U |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D／${ }^{\text {a }}$ | ＝Dipole | turing | 0.000 | 0.0001 | ＋3．2207 |
| d可 | dinit | Diit 1 | 0.000 | 0.2470 |  |
| $\square$ | ＜Quad＞ | Q1 | 0.247 | 0.1398 | ＋13．2014 |
| d可 | difit | difit Q12 | 0.387 | 0.0350 |  |
| $\square^{\circ} \triangle$ | ＜Quad＞ | Q2 | 0.422 | 0.2988 | 8.85920 |
| d可 | dint | difit Q2E | 0.721 | 0.3723 |  |
| E | EElecDip | ElecDip 1 | 1.093 | 1.7453 | ＊450．2kV |
| dㅁ | dinit | dirit ED | 2838 | 1.2250 |  |
| D | ＝Dipole | DipoleA | 4.063 | 0.3491 | －9．6620 |
| F＊ | Fit | F＿DipY | 4.412 | 0.0000 |  |
| F | Fit | F＿DipX | 4.412 | 0.0000 |  |
| S | －sitis＿ | dip silis | 4.412 | 0.0000 |  |
| D2 | ＝Dipole | DipoleB | 4.412 | 0.3491 | －9．6620 |
| d可 | difit | Diitit DE | 4.761 | 1.2225 |  |
| E | ＝ElecDip | ElecDip 2 | 5.984 | 1.7453 | ＊450．2kV |
| 믐 | diit | dinit EQ3 | 7.729 | 0.3649 |  |
| $\square$ | 〈Quad＞ | Q3 | 8.094 | 0.2988 | －5．5964 |
| d可 | diit | difit Q34 | 8.393 | 0.0300 |  |
| $\bigcirc$ | ＜Quad〉 | Q4 | 8.423 | 0.4018 | ＋6．7405 |



Global LISE ${ }^{++}$ matrix with new quad values

| －Global matrix |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| －2．07981 | －0．0736 | 0 | 0 | 0 | －0．22594 | ［mm］ |
| 9.77991 | －0．13474 | 0 | 0 | 0 | 0.45385 | ［mrad］ |
| 0 | 0 | 1.35247 | －1．103e－3 | 0 | 0 | ［mm］ |
| 0 | 0 | 8.96657 | 0.73193 | 0 | 0 | ［mrad］ |
| －0．12657 | 6．385e－3 | 0 | 0 | 1 | 7.90368 | ［mm］ |
| 0 | 0 | 0 | 0 | 0 | 1 | ［\％］ |
| ／［mm］ | ／［mrad］ | ／［mm］ | ［mrad］ | ／［mm］ | ／［\％］ |  |

First order matrix elements
${ }^{100} \mathrm{Se}(1.8 \mathrm{MeV} / \mathrm{u})$; Settings on ${ }^{100} \mathrm{Se}^{20+\ldots 20+}$; Config: DSSSSSESDFFSDSESSSS8FFFFFF ... $\mathrm{dp} / \mathrm{p}=12.75 \%$; Brho(Tm): $0.9662,0.9662,0.9662$





zero angular dispersion

Almost zero
angular dispersion


FP - double focus, double achromatic

## Angular Acceptance

See details for angular acceptance with the next link http://lise.nscl.msu.edu/9 8/SE blocks.pdf\#page=5

## EMMA_beam_AA.Ipp

## Settings

Beam dialog

Monte Carlo options

| Emittance |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| ? | Beam CARD (sigma, semi-axis, hall-width...] |  | 1D - shape (Distribution method) |  |
| 1. $\times$ mm | 0 | Gau | sian | $\checkmark$ |
| 2. T mrad | 100 | Rec | angle uniform | $\checkmark$ |
| 3. $Y \mathrm{~mm}$ | 0 | Gau | sian | $\checkmark$ |
| 4. P mrad | 100 | Rec | angle uniform | $\checkmark$ |
| 5. L mm | 0 | Gaus | sian | $\checkmark$ |
| 6. F | 0 | Gau | sian | $\checkmark$ |

-Angular Acceptance \& Bounds
$\Gamma$ Use fixed angular acceptances
$\checkmark$ Use physical limits (aperture) inside blocks to calculate fragment transmission

For block apertures LISE++ uses the slit limits accessible from the Block Cut \& Acceptance dialog. (Pay attention there for the checkbox

Monte Carlo Transmission settings


## Coming to the FP

Initial emittance gated on the final focal plane
 corresponds to 17 msr (ellipse)

Angular acceptance is equal to $\pm 90 \mathrm{x} \pm 60 \mathrm{mrad}$, that


Gate 2

## EMMA_beam_AA.Ipp


mrad <-> deg.

| Horizontal $\pm$ | 90 |
| :---: | :---: |
| Vertical | 60 |
| Solid angle | 16.96 |

 lost


## Angular Acceptances transmission benchmarks

"Distribution" method
With set Angular Acceptances


"Monte Carlo " method With set Angular Acceptances No bounds

## -Angular Acceptance \& Bounds

V Use fixed angular acceptances
$\lceil$ Use physical limits (aperture) inside blocks to calculate fragment transmission
For block apertures LISE ++ uses the slit limits accessible from the Block Cut \& Acceptance dialog. (Pay attention there for the checkbox

|  |  | N of | N of |  |
| :--- | :--- | :--- | :--- | :--- |
| \# | Ion | Passed | Initial | Transmission |
| All |  | 66579 | 130560 | 51.008 |
| 0 | 100Se | 167370 | 327680 | $51.08 \% \quad(+/-0.12 \%$ |


| Target | 100.08 |
| :--- | :---: |
| tuning | $51.00 \%$ |
| Angular acceptance | $51.00 \%$ |
|  |  |



## "Monte Carlo " method

 No Angular Acceptances WITH boundsAngular Acceptance \& Bounds
$\Gamma$ Use fixed angular acceptances.
V Use physical limits (aperture) inside blocks to calculate fragment transmission
For block apertures LISE++ uses the slit limits accessible from the Block Cut \& Acceptance dialog. (Pay attention there for the checkbox

100Se : Monte Carlo Transmission Plot
$100 \mathrm{Se}(1.8 \mathrm{MeV} / \mathrm{u})+$; Transmitted Fragment 100 $\mathrm{dp} / \mathrm{p}=25.49 \%$; Brho(Tm): 0.9662, 0.9662, 0.9662 AngAccept: Off; Bounds: ON; "FP slits" - last

|  |  | N of | N of |  |
| :---: | :---: | :---: | :---: | :---: |
| \# | Ion | Passed | Initial | Transmission |
| All |  | 85045 | 153693 | 55.338 |
| 0 | 100 Se | 84995 | 153600 | 55.34\% (+/- |




${ }^{100}$ Se : MC Transmission Plot - Envelope (all)
${ }^{100} \mathrm{Se}(1.8 \mathrm{MeV} / \mathrm{u})+$; Transmitted Fragment ${ }^{100} \mathrm{Se}^{20+} .20+$ (beam); Optics Order: 1


Momentum acceptance is defined by the ED1 gap

100Se : Monte Carlo Transmission Plot
after "FP slits": dP/P [\%]: window projection -- $100 \mathrm{Se}(1.8 \mathrm{MeV} / \mathrm{u})+$; Transmitted Fragment $100 \mathrm{Se}^{20+.20+}$ (beam); Optics Order: 1 AngAccept: Off; Bounds: ON; "FP slits" - last block for MC calc; no gates; Config: DSSSSSESDSDSESSSSSSMM
Corresponds to the
Dipole $X$-aperture
$\pm 115 \mathrm{~mm}$

$$
\begin{gathered}
\Delta \mathrm{P} / \mathrm{P}= \pm 7.3 \% \\
(\Delta \mathrm{E} / \mathrm{E}= \pm 14.6 \%)
\end{gathered}
$$

$1^{\text {st }}$ order


Note: Horizontal slits has to be applied for the "Distribution" method to limit momentum acceptance which happens due to apertures.

## Emittance corresponding

 to the acceptances
## "Distribution" method

With set Angular Acceptances and H.slits in MD +/- 130 mm

"Monte Carlo " method; No Angular Acceptances; WITH bounds



| z | N | q | $\mathrm{X}(\mathrm{mm})$ | dx | $\mathrm{X}^{\prime}$ (mrad) | dx' | $\mathrm{Y}(\mathrm{mm})$ | dY | $\mathrm{Y}^{\prime}$ (mrad) | dY' | E,MeVu | dE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 46 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.87555 | 0 |
| 50 | 47 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.85606 | 0 |
| 50 | 48 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.83701 | 0 |
| 50 | 49 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.81829 | 0 |
| 50 | 50 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.8 | 0 |
| 50 | 51 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.782 | 0 |
| 50 | 52 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.76443 | 0 |
| 50 | 53 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.74714 | 0 |
| 50 | 54 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | -34 | 0.1 | 1.73022 | 0 |
| 50 | 46 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.87555 | 0 |
| 50 | 47 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.85606 | 0 |
| 50 | 48 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.83701 | 0 |
| 50 | 49 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.81829 | 0 |
| 50 | 50 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.8 | 0 |
| 50 | 51 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.782 | 0 |
| 50 | 52 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.76443 | 0 |
| 50 | 53 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.74714 | 0 |
| 50 | 54 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0.1 | 1.73022 | 0 |
| 50 | 46 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 34 | 0.1 | 1.87555 | 0 |
| 50 | 47 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 34 | 0.1 | 1.85606 | 0 |
| 50 | 48 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 34 | 0.1 | 1.83701 | 0 |
| 50 | 49 | 20 | 0 | 0 | 0 | 1 | 0 | 0 | 34 | 0.1 | 1.81829 | 0 |
| 50 | 9 different masses@c $0=18$ MV |  |  |  |  |  |  |  | 34 | 0.1 | 1.8 | 0 |
| 50 50 | with Yzangles |  |  | $o f_{0}-2,0, c+2$ |  | degrees |  | (as@ | NIM | $0.1 \mathrm{Fic}$ | $y_{1}^{1.788^{2}}$ | 0 |
| 50 | 53 | 20 | 0 | 0 | - 0 | 1 | 0 | - | 34 | 0.1 | 1.74714 | 0 |
| C- 50 | 18. $5^{54}$ | $\mathrm{Eas}^{20}$ | - ${ }^{0}$ | 0 | 0 | 1 | 0 | 0 | 34 | 0.1 | 1.73022 | 0 |

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Fig. 2. Calculated mass focus of EMMA, showing rays corresponding to 9 adjacent masses emitted from the target with vertical angles of $-2^{\circ}, 0^{\circ}$, and $2^{\circ}$.
At the focal plane, the 9 masses are seen to be dispersed horizontally and focussed vertically. Angular focussing in the horizontal direction is shown in Fig. 4.

LISE++

$2^{\text {nd }}$ order

$1^{\text {st }}$ order

ig. 3. Calculated energy focus of EMMA, showing rays corresponding to a single mass emitted from the target with vertical angles of $-2^{\circ}, 0^{\circ}$, and $2^{\circ}$, and with energies deviating from the central value by $0, \pm 7.5 \%$, and $\pm 15 \%$. Chromatic aberrations in the vertical direction are evident in the vertical extent of the final focus.

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LISE++


Fig. 3 : Benchmarks for Y-angle \&\& Energy (continue)

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## LISE++



## Benchmarks for Y-angle \& Energy (continue 2)

This difference in X-
COSY map of the $1^{\text {st }}$ FMA ED


## After the drift 1.2 m

For $\Delta \mathrm{d}=+7.5 \%$
$\Delta \mathrm{x}=\Delta \mathrm{X}_{1 \mathrm{~d}}+\Delta \mathrm{X}_{2 \mathrm{dd}}+\left(\Delta \mathrm{t}_{1 \mathrm{~d}}+\Delta \mathrm{t}_{2 \mathrm{dd}}\right)^{*} \mathrm{~L}=+85.1 \mathrm{~mm}$
For $\Delta \mathrm{d}=-7.5 \%$
$\Delta \mathrm{x}=\Delta \mathrm{x}_{1 \mathrm{~d}}+\Delta \mathrm{x}_{2 \mathrm{dd}}+\left(\Delta \mathrm{t}_{1 \mathrm{~d}}+\Delta \mathrm{t}_{2 \mathrm{dd}}\right)^{*} \mathrm{~L}=\underline{-105.7 \mathrm{~mm}}$

[^0]
transport format [mm-mrad]

$x_{1 d}=(t / d){ }^{*} \Delta d=4.77 \mathrm{~mm} / \%^{*} 7.5 \%=35 \mathrm{~mm}$
$\Delta \mathrm{x}_{2 \mathrm{dd}}=(\mathrm{x} / \mathrm{d} / \mathrm{d})^{*} \Delta \mathrm{~d} * \Delta \mathrm{~d}=$
$-6.5 \mathrm{e}-2 \mathrm{~mm} / \% / \%$ * $7.5 \%$ * $7.5 \%=-3.7 \mathrm{~mm}$
\[

$$
\begin{aligned}
& \Delta \mathrm{t}_{1 \mathrm{~d}}=(\mathrm{t} / \mathrm{d}) * \Delta \mathrm{~d}=6.7 \mathrm{mrad} / \% * 7.5 \%=50.3 \mathrm{mrad} \\
& \Delta \mathrm{t}_{2 \mathrm{dd}}=(\mathrm{t} / \mathrm{d} / \mathrm{d}) * \Delta \mathrm{~d}^{*} \Delta \mathrm{~d}= \\
& \quad-9.8 \mathrm{e}-2 \mathrm{mrad} / \% / \% * 7.5 \% * 7.5 \%=-5.5 \mathrm{mrad}
\end{aligned}
$$
\]

## Hig. 4 : Benchmarks for X - \& Y -angles

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Y range: $\pm 10 \mathrm{~cm}$

Focal Plane
 emitted from the target with angles of $0, \pm 1.5^{\circ}$, and $\pm 3^{\circ}$ in the vertical and horizontal directions. The dominant geometric aberration in the dispersive direction, proportional to the square of the horizontal angle, is evident in the horizontal extent of the final focus

$2^{\text {nd }}$ order

$2^{\text {nd }}$ order

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Fig. 5. Calculated $M / q$ spectrum of EMMA centred about mass 100 , showing
7 adjacent masses from 97 to 103 emitted from the target with uniform angular spreads of $\pm 3^{\circ}$ in the horizontal and vertical directions, and a uniform energy distribution of $\pm 10 \%$.

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Fig. 5. Calculated $M / q$ spectrum of EMMA centred about mass 100 , showing
7 adjacent masses from 97 to 103 emitted from the target with uniform angular spreads of $\pm 3^{\circ}$ in the horizontal and vertical directions, and a uniform energy distribution of $\pm 10 \%$.

Charge state selection

| Projectile ${ }^{100} \mathrm{Zn}^{\mathbf{3 0 +}}$ |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| fragment |  | ${ }^{100} \mathrm{Zn}^{16+. .16+}$ | =bearm= |
| T ${ }^{\text {P }}$ | Target | ${ }^{2} \mathrm{H}$ |  |
|  |  | 0.0001 | gicir 2 |
| Stor | Stripper |  |  |

Very thin target for charge state simulation with "virtual" A=100 beam

FP slits-Xspace: output after slits
${ }^{100} \mathrm{Zn}(1.8 \mathrm{MeV} / \mathrm{u})+\mathrm{H}\left(1 \mathrm{e}-4 \mathrm{mg} / \mathrm{cm}^{2}\right)$; Settings on $100 \mathrm{Zn}^{16+. .16+}$; Config: DSSSSSESDFFSDSESSSSSFFFFFF. $\mathrm{dp} / \mathrm{p}=100.00 \%$; Brho(Tm): 0.9662, 0.9662, 0.9662




Envelopes : LISE ${ }^{++}$MC \& analytical solutions $\rightarrow X \& Y$

## LISE++ MC




LISE ${ }^{++}$analytical




Envelopes : LISE ${ }^{++}$MC \& analytical solutions $\rightarrow X^{\prime}$ \& $Y^{\prime}$

## LISE++ MC




LISE ${ }^{++}$analytical



| Projectile ${ }^{132} \mathrm{Sn}^{50+}$ $6 \mathrm{MeV} / \mathrm{u} 100 \mathrm{enA}$ |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Fragment ${ }^{133} \mathrm{Sn}^{37+. .37+}$ |  |  |
| To | Target | $\begin{aligned} & \mathrm{H} 2 \mathrm{C} \\ & 0.1 \mathrm{rg}, \mathrm{cr} 2 \end{aligned}$ |
| $\mathbf{S T}^{\text {a }}$ | Stripper |  |

## EMMA_reaction_NoGold.Ipp

Without gold degrader


## Production mechanism

- Two Body Reactions:
$5 \cdot[<15 A M e V]$ G.Schiwietz, P.Grande, NIM B175-177 (2001) 125-131

Energy Losses
$1 \cdot[\mathrm{H}$-base] J.F. Ziegler et al, Pergamon Press, NY (low energy)

Reaction $\mathrm{d}\left({ }^{132} \mathrm{Sn}, \mathrm{p}\right)^{133} \mathrm{Sn}$ : fragment distributions

${ }^{132} \mathrm{Sn}(6.0 \mathrm{MeV} / \mathrm{u})+\mathrm{H} 2 \mathrm{C}\left(1 \mathrm{e}-1 \mathrm{mg} / \mathrm{cm}^{2}\right)$


Please, Compare with Fig. 6 NIMA paper


$$
\begin{aligned}
& Q=41^{+} \text {and energy } 782 \mathrm{MeV} \\
& \text { are indicated in NIMA paper }
\end{aligned}
$$

133Sn after Target (H2C): Fragment energy $=5.8$
${ }^{132} \mathrm{Sn}(6.0 \mathrm{MeV} / \mathrm{u})+\mathrm{H} 2 \mathrm{C}\left(1 \mathrm{e}-1 \mathrm{mg} / \mathrm{cm}^{2}\right)$
Calculations for ${ }^{133} \mathrm{Sn}{ }^{37+37+37+37+37+}$; Material H 2 C


## Reacilon d(132Sn, $133 \mathrm{~S} \cap$ (with gold degrader)



| D | DipoleB |  | $\begin{gathered} \text { Brho } \\ 0.9862 \mathrm{Tm} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| dㅁ | drift DE |  | standard $1.22 \text { m }$ |
| E二 | ElecDip 2 | Er | $4371.5 \mathrm{kV} / \mathrm{m}$ 546.4 KV 21.86 MJJC |

$\mathrm{Q}=37^{+}$(????? $)$and energy 463 (??) MeV are indicated in NIMA paper
${ }^{133}$ Sn distributions after the gold degrader



Reaction $d\left({ }^{132} \operatorname{Sn}, \mathrm{p}\right)^{133} \mathrm{Sn}$ (with god degrader)

| MICHIGAN STATE |
| :--- |
| 1 N |

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## "Distribution" method (analytical solution)

| 푼 statistics: 133Sn |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 133Sn Beta | Beta- decay ( $\mathrm{Z}=50, \mathrm{~N}=83$ ) |  | Tin |  |
| All reactions total isotope rate $181 \mathrm{et3}$ <br> and Overall isotope transmission 59.472 |  |  | $\begin{aligned} & \text { pps } \\ & \stackrel{\text { \% }}{8} \\ & \hline \end{aligned}$ |  |
| Q1 (tuning) |  | 32 | 31 | 30 |
| Q2 (ElecDip 1) |  | 32 | 31 | 30 |
| Q3 (DipoleA) |  | 32 | 31 | 30 |
| Q4 (DipoleB) |  | 32 | 31 | 30 |
| Q5 (ElecDip 2) |  | 32 | 31 | 30 |
| Reaction |  | TwoBod | TwoBody | TwoBody |
| Ion Production Rate | (pps) | $6.19 \mathrm{e}+$ | $6.65 \mathrm{e}+2$ | $5.26 \mathrm{e}+2$ |
| Total ion transmission | (\%) | 20.336 | 21.853 | 17.282 |
| Total: this reaction | (pps) | $1.81 \mathrm{e}+$ | $1.81 \mathrm{e}+3$ | $1.81 \mathrm{e}+3$ |
| X -Section in target | (mb) | $2.16 \mathrm{e}+$ | $2.16 \mathrm{e}+1$ | $2.16 \mathrm{e}+1$ |
| Target | (8) | 100 | 100 | 100 |
| Unreacted in material | (\%) | 100 | 100 | 100 |
| Unstopped in material | (\%) | 100 | 100 | 100 |
| Stripper | (8) | 20.34 | 21.85 | 17.28 |
| Unreacted in material | (\%) | 100 | 100 | 100 |
| Q (Charge) ratio | (\%) | 20.34 | 21.85 | 17.28 |
| Unstopped in material | (\%) | 100 | 100 | 100 |

## FP slits-Xspace: output after slits




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## Open Questions:

1. Mass \& charge dispersion values calculation
2. Using Mass \& charge dispersion values for optimization
3. Electrical dipole second order matrix calculation! (new)

[^0]:    !!! Electric dipole $x / d^{2} \& t / d^{2}$ values are very important for the analyzer and should calculated by LSE ${ }^{++}$in future

